



Removal of Arsenic from Groundwater with Low Cost Multilayer Media

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Abstract

A simple, low cost arsenic removal system was developed to treat arsenic contaminated ground water containing 425 ± 4.2 $\mu\text{g/L}$ arsenic. The system decontaminates arsenic from water by sorption through fine particles of waste materials (Coconut husk's ash, Refused brick dust, Stone dust and Waste newspaper) of multilayer. The treatment efficiency of the process was investigated under various operating conditions that might affect the sorption/ desorption of arsenic. Sorption column method shows the optimum removal of As(III) under the following conditions: initial As concentration (100 $\mu\text{g/L}$), sorbent amount (4.0 g for brick dust, 3.0 g for stone dust, 3.0 g for Coconut husk's ash and 0.3 g for waste newspaper), particle size (<355 μm), treatment flow rate (1.4 mL/min), optimum volume (100 mL) and pH (5.0). Desorption efficiencies with 2M of KOH after the treatment of groundwater were observed in the range of $78 \pm 1.2\%$ - $82 \pm 1.4\%$. Average arsenic concentration of treated sample water was 8.30 ± 0.4 $\mu\text{g/L}$ which is below the WHO guideline value for Bangladesh. Different techniques were used to measure thirteen metals, four anions with pH, conductivity, and temperature to understand the status of other species before and after treatment. The average concentrations of other inorganic constituents of health concern (Cu, Mn, Pb, Cr and Fe) in treated water were below WHO guideline value for drinking water. The present study showed a new method for removal of as from ground water.

Keywords: Arsenic; Removal; Sorption; Low cost; Multilayer.

Introduction

Arsenic pollution is one of the serious water contaminations of drinking water. It is a ubiquitous element which ranked 20th in natural abundance, comprising about 0.00005% of earth crust, 14th in sea water and 12th in human body [1]. It is found in the atmosphere, soils, rocks and natural organisms. Natural processes including soil erosion, mineral leaching and weathering are responsible for introducing arsenic into surface waters [2]. Soil erosion and leaching contribute to 612×10^8 g/year and 2380×10^8 g/year of arsenic respectively, in dissolved and suspended forms in the ocean. Arsenic occurs as organic and inorganic compounds in natural water. It is found that arsenic toxicity depends on its oxidation state. Arsenites As(III) are ten times more toxic for biological systems than arsenates. The inorganic forms of

arsenic are more toxic than organic-arsenic compounds.

The prolonged exposure of humans to nonlethal arsenic dose causes chronic health effects, but long time exposure usually causes death. The arsenic calamity of Bangladesh can be described as the largest known mass poisoning in the history, with an estimated 35–77 million people exposed to arsenic-contaminated drinking water [3]. About 61% of the tube wells water has arsenic content above 0.05 mg/L and about 13% have arsenic content above 10 $\mu\text{g/L}$ [4]. This is significantly higher than the World Health Organization (WHO) maximum permissible limit in drinking water (50 $\mu\text{g/L}$). The Environmental Protection Agency (EPA) has

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recently adjusted the upper limit of arsenic $10\mu\text{g/L}$ in drinking water.

Arsenic can be removed from aqueous solution by using many technologies such as ion exchange resin, activated alumina, coprecipitation with iron or alum, reverse osmosis, membrane filtration, modified coagulation/filtration, and enhanced lime softening etc [5-8]. However, none of these technologies are currently applied on a broad scale in developing countries like Bangladesh as they require sophisticated technical systems and are therefore unpractical in low income regions. Among these methods, the adsorption techniques are simple and convenient for regeneration and sludge free operation. So far, various adsorbents for arsenic removal have been developed that include materials such as metal-loaded coral limestone [14], hematite and feldspar [16] activated carbon and activated alumina [15], hydrous zirconium oxide, rice husk [9] sawdust and oyster shell [13]. However, most of these adsorbents entail several problems in terms of efficiency and cost [9].

The present work was aimed to develop a cost effective and simple method for arsenic decontamination from drinking water. Various chemical parameters in water before and after treatment were measured. The sorbents used in these experiments were waste materials. They were available and cheap. They were found to have tremendous arsenic uptake capacity.

Experimental

Reagents

All reagents used throughout this work were of analytical-grade purity. Arsenic (III) standard solution of 1000 mg/L was procured from Kanto Company, Japan and NaOH, KOH, HCl, HNO_3 , and H_2SO_4 were obtained from Merck, Germany. Stock solution (10 mg/L) of As(III) was prepared in de-ionized water from Arsenic(III) standard solution of 1000 mg/L . Dilute standard solutions were freshly prepared.

Preparation of sorbents

Four types of sorbents were used. These were coconut husk's ash, refused brick dust, stone

dust and used newspaper. The newspaper used in the present work was obtained from a university dormitory which contains large amount of cellulose. Coconut husk's ash was collected from Darichar Luxmipur village of Madaripur district. Stone dust and Refused brick were collected from respective sites of Dhaka city. Sorbents were washed by water several times to remove dust and fine particles. The washed materials were then dried in a hot-air oven (NDO-450ND, EYELA, Japan) at 110°C for 24 hours. The washed dried materials were grinded and sieved into the following three size fractions ($600\text{-}425\mu\text{m}$, $425\text{-}355\mu\text{m}$ and $<355\mu\text{m}$). Coconut husk's ash was dried only and its particle size was only $<355\mu\text{m}$. Newspaper was shredded into small pieces and then dried. Before using into column, it was soaked with water for 24 hours and then shredded again to make into paste like substance and finally washed with water three times to make ink free. All materials were used for the removal of arsenic without any chemical pretreatment. To make a multilayer, firstly the particle sizes and amount of sorbents were optimized. Each sorbent of optimized amount was placed in the column and water was passed through it to remove dust and dissolved substances. Similarly other sorbents were added successively.

Arsenic removal experiment in column

For individual treatment, all sorbents except newspaper, ($2.0\text{-}6.0\text{ g}$) were added to the treatment glass column ($2.5\text{ cm} \times 30\text{ cm}$). Newspaper was added ($0.1\text{-}0.5\text{ g}$). Sorption experiments were carried out in a column that was equipped with a stopper for controlling the column effluent flow rate (treatment rate). Sorption factors including the amount of sorbents ($0.1\text{-}6.0\text{ g}$, particle size ($<355\text{-}600\mu\text{m}$), treatment flow rate ($1.0\text{-}2.2\text{ mL/min}$), initial As concentration ($300\text{-}1000\mu\text{g/L}$), and pH ($1\text{-}12$) were evaluated. The packing density of refused brick dust ($<355\mu\text{m}$) was 0.96 g/cm^3 , Stone dust ($<355\mu\text{m}$) was 1.25 g/cm^3 , Coconut husk's ash was 0.58 g/cm^3 and waste news paper was 0.36 g/cm^3 . Small amount of glass wool was inserted into the bottom of the column to prevent the loss of sorbents during the treatment. The flow rate was kept constant by controlling the stopper valve. The removal (sorption)

efficiency was calculated by using the following equation:

$$\text{Removal (sorption) efficiency} = [(C_0 - C_e) / C_0] \times 100$$

Where, C_0 and C_e are the concentration of As in the sample solution before and after treatment, respectively.

Analysis of arsenic

The treated and nontreated sample solutions were analyzed using Hydride Vapor Generator (HVG) attached with Atomic Absorption Spectrophotometer (AAS-680, Shimadzu, Japan) for the determination of total arsenic followed by the generation of arsine gas (AsH_3).

Sodium borohydride solution

3.0 g of sodium hydroxide and 2.5 g of sodium borohydride (both were analar grade) were dissolved in distilled deionized water and finally volume of the solution was adjusted to 500 mL by adding deionized water.

Hydrochloric acid solution

Concentrated hydrochloric acid (37%, analar grade) was diluted to make 500 mL of 5M HCl.

Preparation of standard arsenic solution

From 10 mg/L stock solution, 1-5 $\mu\text{g/L}$, 100 mL of As^{3+} solutions were prepared. The standard solutions were aspirated in HVG – AAS and a calibration curve was prepared.

Analysis of samples

The treated samples were diluted to a known volume after adding 2.0 g of KI and 2.0 ml of concentrated HCl in each of the sample solutions. Samples were then allowed to stand for two hours and were analyzed by HVG-AAS [10]. The samples were analyzed against a calibration curve prepared by the standard solutions of arsenic. Each unknown sample was analyzed three times.

Analysis of Na, K, Ca, Mg, Cu, Mn, Cr, Pb and Fe

Na, K, Ca, Mg, Cu, Mn, Cr, Pb and Fe were analyzed using Flame Atomic Absorption Spectrophotometer. (Model: AA-680, Shimadzu, Japan) [10]. Precision and analytical accuracy of the methods were evaluated by standard reference material, Wheat flour, SRM 8437 (National Institute of Standard and Technology, USA).

Analysis of Cl^- , PO_4^{3-} , NO_3^- and SO_4^{2-}

Cl^- , PO_4^{3-} , NO_3^- and SO_4^{2-} from the treated and untreated samples were analyzed by UV-visible spectrophotometric method [10].

Results and Discussion

Initially four different sorbents were selected and arsenic solution of 100 mL (pH~6.7) and 100 $\mu\text{g/L}$ was passed through 5.0 g of each sorbent and removal efficiency was evaluated. Removal efficiency of coconut husk's ash was $94.8 \pm 0.6\%$, stone dust $88.50 \pm 0.8\%$, for brick dust $84.72 \pm 1.2\%$. The performances of sorbents were evaluated for the removal of As (III). Preliminary studies showed that the complete removal of As(III) was achieved under the following conditions: particle size $<355 \mu\text{m}$, amount of coconut husk's ash, 3.0 g; stone dust, 4.0 g; brick dust 4.0 g and newspaper 0.3 g.

Effect of particle size

Column sorption experiments were carried out for the removal of As(III) from aqueous solution using three different particle sizes [$<355\mu\text{m}$, (355-425) μm and (425-600) μm] with the constant amount of sorbents (5.0g) of both stone dust and brick dust. Removal efficiency of arsenic was found decreased with increasing particle size. As the size of the sorbent particles increased, the sorption of metal ions decreased. Lower particle size provides higher surface area for arsenic to be accumulated.

Effect of the amount of sorbents

The effect of the amount of sorbents on the removal of As(III) was investigated. The results

were presented in (Fig. 1). For all sorbents (coconut husk's ash, stone dust, brick dust and newspaper) removal efficiencies of As(III) were increased gradually with the increase of amount of sorbents up to a certain level. Then removal efficiency was not changed significantly. Sorbent's sorption capacity was depended on the surface activity such that specific surface area available for As-surface interactions that was accessible to the As(III). At higher amount of sorbent, surface area was decreased due to agglomeration of the same sorbent particles. Considering the removal efficiencies of the sorbents, 4.0 g of both stone dust and refused brick, 3.0 g of coconut husk's ash and 0.3 g of newspaper were chosen for next study.

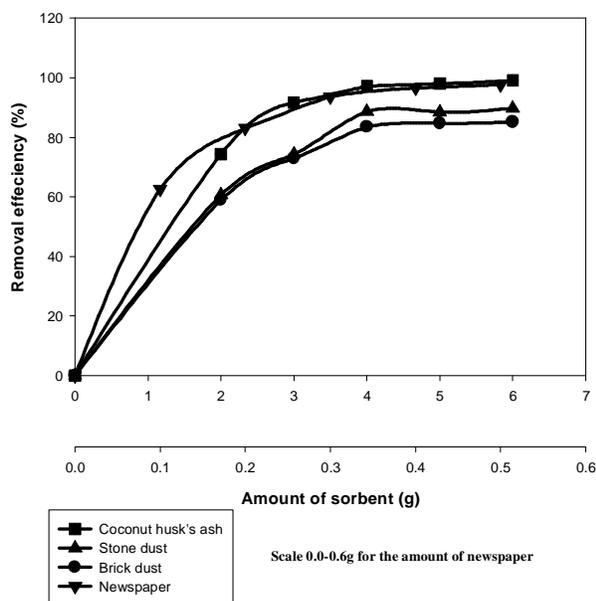


Figure 1. Effect of sorbent's amount on the removal of As(III) by adsorption onto Coconut husk's ash, stone dust, brick dust, newspaper.

Initial concentration of Arsenic solution, 100 $\mu\text{g/L}$
 Volume of sorbate solution, 100 mL
 Flow rate, 0.6 mL/min

Formation of multilayer

By using these optimized amounts of different sorbents a multilayer was prepared. Order of sorbents was chosen arbitrarily. The different multilayer were assigned by block letters (A, B, C, D and E) and presented in Table 1. Arsenic solution of concentration 400 $\mu\text{g/L}$ and volume 100 mL was passed through each column. Results were represented in (Fig. 2). It shows that multilayer 'D' has the highest arsenic removal

efficiency which was 98.48%. It was notable that when arsenic solution was treated individually with sorbent, the average removal efficiency of optimized amount of sorbents was about $90 \pm 1.2\%$. However, multilayer showed $98.48 \pm 1.6\%$ removal efficiency. Therefore, the removal efficiency was improved due to the formation of multilayer. It was due to the availability of fresh active sites in multilayer where arsenic was adsorbed successively. In multilayer D, coconut husk's ash was at the bottom layer which had highest removal efficiency, made possible to remove the remaining arsenic effectively.

Table 1. Order of sorbents in multilayer (Bottom layer to top layer).

| No of multilayer | Order of sorbents | Symbol |
|------------------|---|--------|
| 1 | Brick dust/ stonedust/coconut husk's ash/ newspaper | A |
| 2 | Stonedust/ brick dust/ coconut husk's ash/ newspaper | B |
| 3 | Newspaper/ coconut husk's ash / Stonedust/ Brick dust | C |
| 4 | Coconut husk's ash / Brick dust/ Stonedust/ newspaper | D |
| 5 | Coconut husk's ash / Stonedust/ Brick dust/ newspaper | E |

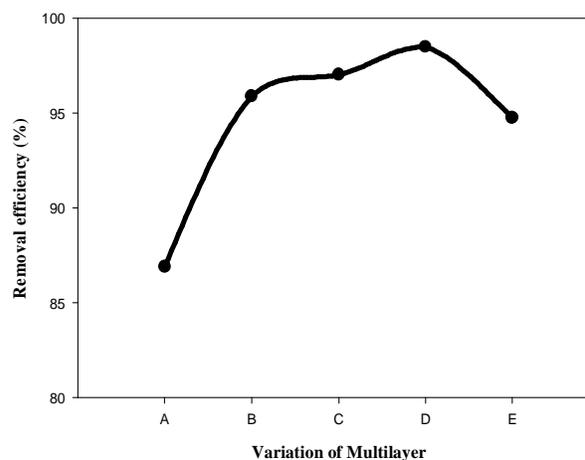


Figure 2. Comparison of relative removal efficiency of various Multilayer.

Initial conc. of Arsenic solution, 400 $\mu\text{g/L}$
 Volume of sorbate solution, 100 mL
 Particle size, <355 μm
 Flow rate, 0.6 mL/min

A= Brick dust/ stonedust/coconut husk's ash/ newspaper
 B=Stonedust/ brick dust/ coconut husk's ash/ newspaper
 C=Newspaper/ coconut husk's ash / Stonedust/ Brick dust
 D=Coconut husk's ash / Brick dust/ Stonedust/ newspaper
 E= Coconut husk's ash / Stonedust/ Brick dust/ newspaper

Effect of flow rate

The effect of flow rate on the removal of As(III) was examined. It was observed that removal efficiency decreased with increasing flow rate. Removal efficiency varied from $98 \pm 0.8\%$ to $91 \pm 1.1\%$ with increasing flow rate from 1.0 mL/min to 2.2 mL/min. When the flow rate was slow, As(III) in the sample solution got more contact time with the active surface of the sorbents in the multilayer. So, the probability of interactions was higher.

Effect of initial concentration

For the evaluation of the effect of initial concentration, 100 mL solution of various concentrations of As(III) was treated onto the multilayer. The results were illustrated in (Fig. 3) which showed that removal efficiency decreased with increasing initial concentrations. The removal efficiency of Arsenic decreased from $99 \pm 2.0\%$ to $75 \pm 0.6\%$ with the increase of initial concentration from $300\mu\text{g/L}$ to $1000\mu\text{g/L}$. At low concentration, most of the As(III) in the solution got enough active sites of sorbent but with increase of concentration, all As(III) species were not able to come in contact with active sites of sorbents.

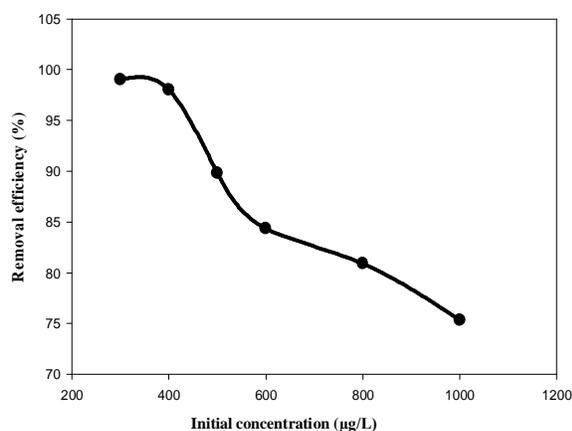


Figure 3. Effect of initial sorbate concentration on the removal of As(III) by sorption onto Multilayer.

Volume of Arsenic solution, 100 mL
Flow rate, 1.4 mL/min
Particle size, <355 µm
Multilayer, D (Coconut husk's ash / Brick dust/ Stone dust/ newspaper)

Effect of initial volume

Different initial volumes with optimized concentration $400\mu\text{g/L}$ As(III) solution were treated onto multilayer and results were summarized in (Fig. 4). It shows clearly that removal efficiency decreases with increase of initial volume. The removal efficiency varied from $99 \pm 1.7\%$ to $59 \pm 0.3\%$ with initial volume 50 mL to 200 mL. This removal efficiency was decreased due to the less availability of active sites to get contact of multilayer. Less volume of solution contains less amount of arsenic; as a result most of arsenic got available sorbent sites.

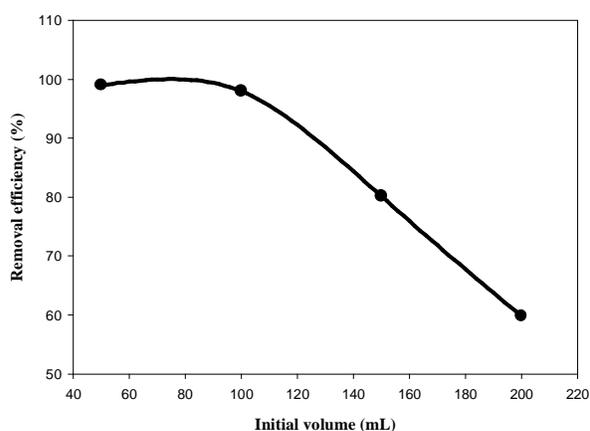


Figure 4. Effect of sorbate volume on the removal of As(III) by sorption onto Multilayer.

Initial concentration of Arsenic solution, $400\mu\text{g/L}$
Flow rate, 1.4 mL/min
Particle size, <355 µm
Multilayer, D (Coconut husk's ash / Brick dust/ Stone dust/ newspaper)

Effect of pH

pH is one of the most important parameters controlling the metal ion sorption process [11]. The pH will determine whether the ionized or unionized sorbate species will exist in solution as well as the degree of ionization of surface functional groups. Sorption experiments were carried out at different pH (1-12) and (Fig. 5) described the effect of pH on As(III) removal with sorbent. The efficiency curve was a hump shape. Highest removal efficiency was found at pH 5. It is due to the existence of H_2AsO_4^- species at this pH, which is suitable for adsorption rather than neutral species. Moreover, waste newspaper, alumina and iron oxide have greater

accumulation capacity at this pH due to the formation of $C-OH_2^+$, $AlOOH$ and $FeOOH$ species which act as potential arsenic sorbent sites [12].

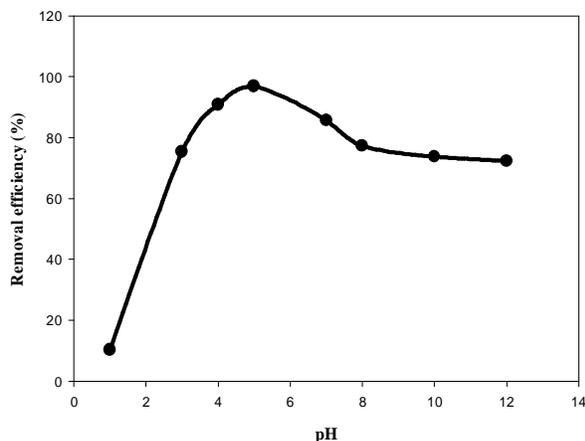


Figure 5. Effect of pH on the removal of As(III) by sorption onto Multilayer.

Initial concentration of Arsenic solution, 400 $\mu\text{g/L}$
 Volume of Arsenic solution, 100 mL
 Flow rate, 1.4 mL/min
 Multilayer, D (Coconut husk's ash/Brick dust/Stone dust/ newspaper)

Desorption

In order to recover arsenic from sorbents for its safe disposal as well as keeping the process cost low, the possibility of desorption in many cases is as important as sorption. Desorption experiments were carried out at different concentration of acids and bases and were presented in Table 2. Attempts were made to desorb As(III) from the sorbents surface with various eluents, such as HCl, HNO_3 , NaOH and KOH. This desorption process was performed using the batch method. Desorption efficiency of arsenic tends to increase with increasing standing time. Acid desorption was problematic because it degraded the sorbents used for sorption. Potassium hydroxide solution was useful for the desorption of arsenic from the surface of sorbents. In both acidic and basic conditions, highest desorption was achieved from 86 to 87% rather than 100%. It is indicative that some strong chemical bond was formed during sorption between arsenic and sorbents which could not be removed by desorption.

Table 2. Influence of the Eluent on the Desorption of As(III) .

| Eluating agent | Standing time (h) | Desorption (%) |
|---------------------|-------------------|----------------|
| KOH (1M) | 8 | 70 \pm 1.6 |
| | 16 | 71 \pm 0.9 |
| | 20 | 74 \pm 1.1 |
| KOH (2M) | 8 | 78 \pm 1.2 |
| | 12 | 81 \pm 1.2 |
| | 18 | 82 \pm 1.4 |
| KOH (4M) | 1 | 85 \pm 1.2 |
| | 2 | 87 \pm 1.5 |
| NaOH (1M) | 8 | 58 \pm 0.7 |
| | | 45 \pm 1.1 |
| HNO_3 (1M) | 0.5 | 51 \pm 0.8 |
| | 1.0 | 65 \pm 0.9 |
| HNO_3 (2M) | 0.33 | 77 \pm 0.8 |
| | 1.0 | 84 \pm 1.7 |
| HNO_3 (4M) | 0.33 | 86 \pm 1.3 |
| | 1.0 | |

Initial As concentration: 400 $\mu\text{g/L}$
 Volume of arsenic solution: 100 mL
 Treatment flow rate: 1.4 mL/min
 Volume of desorption agent: 100 mL

Applicability of the developed system

All the optimized conditions for arsenic removal were presented in Table 3. The utility of the developed method was evaluated for the treatment of As contaminated groundwater samples of Bangladesh. The concentrations of total arsenic in nontreated sample waters were $431.00 \pm 4.2 \mu\text{g/L}$, $408.53 \pm 4.8 \mu\text{g/L}$ and $436.88 \pm 3.6 \mu\text{g/L}$. The treatment results were presented in Table 4. (4 g stone dust + 4 g brick dust + 3 g coconut husk's ash + 0.3.0 g newspaper) = 11.3 g of sorbent was applied in each treatment; the concentrations of arsenic in the treated sample water were lowered to $8.50 \pm 0.5 \mu\text{g/L}$, $8.15 \pm 0.2 \mu\text{g/L}$ and $8.26 \pm 0.6 \mu\text{g/L}$. The desorption efficiencies with 100 mL of 2 M KOH were 84 \pm 1.5%, 80 \pm 1.4% and 82 \pm 1.7%. therefore arsenic can be successfully removed from real As-contaminated groundwater, and the adsorbed As could be recovered from the surface of multilayer.

The status of other chemical and physical parameters in ground water before and after treatment was analyzed and was compared with WHO and Bangladesh guideline value and presented in Table 5.

Table 3. Optimized conditions for removal of arsenic onto multilayer.

| Run no | pH | Concentration of As in nontreated water ($\mu\text{g/L}$) | Concentration of As in treated water ($\mu\text{g/L}$) | Removal efficiency (%) | Desorption (%) |
|--------|------|---|--|------------------------|----------------|
| 1 | 8.20 | 431.00 \pm 4.2 | 8.50 \pm 0.5 | 98.02 \pm 3.7 | 84 \pm 1.5 |
| 2 | 8.15 | 408.53 \pm 4.8 | 8.26 \pm 0.2 | 97.99 \pm 4.6 | 80 \pm 1.4 |
| 3 | 8.26 | 436.88 \pm 3.6 | 8.15 \pm 0.6 | 98.13 \pm 3.0 | 82 \pm 1.7 |

Table 4. Removal and Desorption of As from the Contaminated water by the Developed Method.

| Name of the parameter | Optimized value |
|---------------------------------|--|
| Particle size | <355 μm |
| Sorbent amounts for multilayer | 3.0, 4.0, 4.0 and 0.3 g for coconut husk's ash, stone dust, brick dust and newspaper respectively. |
| Order of sorbents in multilayer | Coconut husk's ash/ Brick dust/ Stone dust/ newspaper |
| Flow rate | 1.4 mL/min |
| Initial concentration | 400 $\mu\text{g/L}$ |
| Initial volume | 100 mL |
| pH | 5.0 |
| Desorption | 2M KOH |

No of analysis for each sample (n)=3

Particle size : <355 μm

Flow rate: 1.4 mL/min

Desorption: 2 M KOH, 100 mL

Standing time: 10 hour

Multilayer D (Coconut husk's ash / Brick dust/ Stone dust/ newspaper)

Table 5. Comparison of some water quality parameters of nontreated and treated water with guideline value.

| Parameter | Nontreated water (mg/L) | Standard deviation \pm | Treated water (mg/L) | Standard deviation \pm | Bangladesh Govt guideline value (EQS 1997) (mg/L) | WHO guideline value (mg/L) |
|-----------------|-------------------------|--------------------------|----------------------|--------------------------|---|----------------------------|
| Arsenic | 0.425 | 0.0042 | 0.008 | 0.0004 | 0.05 | 0.01 |
| Iron | 8.50 | 0.002 | BDL | - | 0.3-1.0 | 0.30 |
| Manganese | 1.55 | 0.001 | BDL | - | 0.1 | 0.05 |
| Lead | 0.003 | 0.05 | BDL | - | 0.05 | 0.01 |
| Cadmium | 0.39 | 0.02 | BDL | - | 0.005 | 0.003 |
| Chromium | 0.001 | 0.3 | BDL | - | 0.05 | 0.05 |
| Zinc | 0.02 | 0.18 | 0.002 | 0.07 | 5.0 | 3.0 |
| Copper | 0.01 | 0.30 | 0.10 | 0.01 | 1.0 | 1.0 |
| pH ^b | 8.20 | 0.001 | 9.32 | 0.04 | 6.5-8.5 | 6.5-8.5 |
| TDS | 527.0 | 2.50 | 65.10 | 2.45 | 1000 | 1000 |
| Sodium | 18.45 | 0.66 | 14.10 | 1.22 | 200 | 200 |
| Calcium | 192.25 | 1.70 | 15.32 | 1.26 | | |
| Silver | 0.001 | 0.03 | BDL | - | | |
| Potassium | 3.43 | 1.2 | 39.85 | 0.74 | 12 | 10 |
| Phosphate | 0.030 | 0.01 | 0.008 | 0.02 | | |
| Sulphate | 0.62 | 0.04 | 0.06 | 0.01 | | |
| Chloride | 2.5 | 0.22 | 0.05 | 1.60 | | |
| Nitrate | 0.96 | 0.30 | 0.06 | 0.21 | 10 | 50 |

BDL=Below Detection Limit, b=unitless

Conclusion

The proposed column treatment system is appropriate and suitable homemade approach for arsenic removal in local areas, because of its simplicity and easy operation and handling. As waste materials are easily available and cheap, the proposed method is very suitable for the poor people of rural areas of developing country like Bangladesh. It is effective for a wide range of concentrations, which were quite similar to those observed in contaminated Bangladeshi groundwater. No secondary pollution problem will occur because desorption of arsenic is possible. Direct removal of both arsenite and arsenate can be achieved. Most of the arsenic contaminated areas are in the villages and the socio-economic conditions of the people are very low. Hence, they need a cost effective method for arsenic removal, whereas the traditional methods require the oxidation process. Thus, waste sorbents in the form of multilayer would become promising, simple, cost effective sorbents for the removal of arsenic.

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